



# Introduction to *Geometric Modeling*

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Ship Design I

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## Summary

1. Parametric Curves
2. Parametric Surfaces

## Parametric Curves

### 1. Mathematical Formulations

- Cubic Splines
- Bézier
- B-Spline
- Beta-Spline
- NURBS

### 2. Interpolation and approximation of curves

### 3. Analysis of curves

## Cubic Spline (1)

Considering the wooden spline (*virote*) a thin elastic beam, and for small deflections, the Euler law relates the deflection of the beam axis  $y(x)$  with the bending moment  $M(x)$  by the expression:

$$y''(x) = \frac{M(x)}{EI}$$

where:

E - Modulus of Young

I - Moment of inertia of the beam section





## Cubic Spline (2)

- Assuming that the beam is simply supported on the weights, then the bending moment varies linearly between them, i.e.,  $M(x) = Ax + B$ . Replacing in the expression and integrating results

$$y(x) = \iint \frac{M(x)}{EI} dx = \frac{1}{EI} \iint (Ax + B) dx = Ax^3 + Bx^2 + Cx + D$$

In each segment, the curve can be defined as a function of the parameter  $t$  normalized for the interval  $[0,1]$

$$P(t) = At^3 + Bt^2 + Ct + D$$

The constants can be obtained from the following boundary conditions:

$$\begin{cases} P(0) = p_0 \\ P(1) = p_1 \\ P'(0) = T_0 \\ P'(1) = T_1 \end{cases}$$

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5



## Cubic Spline (3)

Finally the curve can be represented in the matrix form as

$$P(t) = \begin{bmatrix} t^3 & t^2 & t & 1 \end{bmatrix} [H] [G]$$

where

$$[H] = \begin{bmatrix} +2 & -2 & +1 & +1 \\ -3 & +3 & -2 & -1 \\ 0 & 0 & +1 & 0 \\ +1 & 0 & 0 & 0 \end{bmatrix} \quad [G] = \begin{bmatrix} p_i \\ p_{i+1} \\ T_i \\ T_{i+1} \end{bmatrix}$$

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## Bézier Curves (1)

- The curves generally known as Bézier resulted from separate research from Casteljaou (Citroen) and Pierre Bézier (Renault) in the beginning of the 1960s.
- A Bézier curve is defined by:

$$P(t) = \sum_{i=0}^n C_i B_{n,i}(t) \quad \text{for } 0 \leq t \leq 1$$

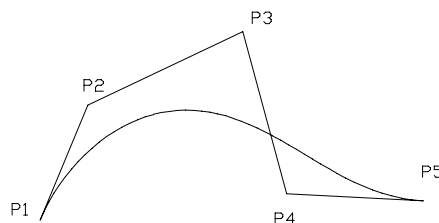
where  $B_{n,j}$  are the Bernestein base functions, of degree  $n$

$$B_{n,i} = \frac{n!}{i!(n-i)!} (1-t)^{n-i} t^i$$

$$= \binom{n}{i} (1-t)^{n-i} t^i \quad \text{for } i = 0, 1, \dots, n$$

## Bézier Curves (2)

- The Bézier curve is tangent to the first and last segments of the control polygon
- The curve order is equal to the number of vertices of the control polygon.
- The curve is entirely contained in the convex hull of the control points.





## B-Spline Curves (1)

- They were studied by N. Lobatchevsky in the XIX century
- Their use for curve fitting to experimental data began in 1946 with Schoenberg
- They were first introduced in CAD systems by J. Ferguson (Boeing) in 1963.

$$C_k(t) = \sum_{i=0}^n P_i N_{i,k}(t)$$

Where  $C_i$  are the points of the control polygon and  $N_{i,k}$  are the B-Spline base functions, of order  $k$ , that can be computed by the recursive expression from Cox/de Boor:

$$N_{i,0}(t) = 1 \quad \text{para} \quad t_i \leq t < t_{i+1}$$

$$= 0$$

Defined over a knot vector

$$N_{i,k}(t) = \frac{t - t_i}{t_{i+k} - t_i} N_{i,k-1}(t) + \frac{t_{i+k} - t}{t_{i+k} - t_{i+1}} N_{i+1,k-1}(t)$$

$$X = \{t_1, t_2, t_3, \dots, t_m\}$$

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9



## B-Spline Curves (2)

- The knot vector is a non-decreasing sequence of numbers
- The knot vector can be classified as:
  - Uniform - the increment between knots is constant  
{ 0.0, 0.5, 1.0, 1.5, 2.0 }
  - Periodic - the increment is constant and equal to 1  
{ 0, 1, 2, 3, 4, 5 }
  - Non-Periodic - the increment of the interior knots constant and equal to 1 and the knots of the extremities with multiplicity equal to the order  
{ 0, 0, 0, 1, 2, 3, 4, 5, 5, 5 }
  - Non-Uniform - the increment of the interior knots not necessarily constant and the knots of the extremities with multiplicity equal to the order  
{ 0, 0, 0, 1.0, 1.4, 2.0, 2.3, 3.0, 3.0, 3.0 }

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10



## B-Spline Curves (3)

The B-Spline curves have the following properties:

- Linear precision
- Convex hull, in  $k$  consecutive control points
- Variation diminishing
- Are invariant when submitted to affine transformations
- When the order of the B-Spline is equal to the number of control points, the knot vector consists only in the values of the extremities with the multiplicity equal to the order

$$\{ 0, 0, 0, 0, 1, 1, 1, 1 \}$$

and the B-Spline base functions are equivalent to Bernstein functions and the curve degenerates into a Bézier curve.



## Beta-Splines (1)

- Os cubic Beta-splines were introduced on 1981 by Barsky
- They are a generalization of the B-Splines based in notions of geometric continuity and in the mathematical modeling of tension
- The requirements of parametric continuity of the 2<sup>a</sup> order ( $C^2$ ) between the B-Splines segments is replaced by the requirements of geometric continuity of 2<sup>a</sup> order ( $G^2$ ) of the unit tangent vector and of the curvature vector
- This originates discontinuities of the 1st and 2nd parametric derivative, that are expressed as functions of the parameters  $\beta_1$  and  $\beta_2$ , designated by bias and tension, respectively.

## Beta-Splines (2)

- A Beta-spline curve is defined by:

$$C_i(u) = \sum_{r=-2}^1 b_r(\beta_1, \beta_2; u) P_{i+r} \quad p/0 \leq i < 1$$

where  $b_r$  are the base functions

$$b_r(\beta_1, \beta_2; u) = \sum_{g=0}^3 c_{gr}(\beta_1, \beta_2) u^g \quad p/0 \leq u < 1 \quad r = -2, -1, 0, 1$$

- The parametric continuity reflects the fair variation of the parameterization and not necessarily of the curve
- The geometric continuity is a measure of the continuity that is independent from the parameterization

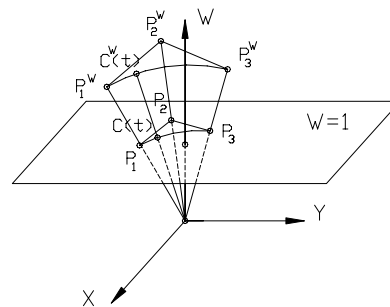
## NURBS Curves

$$C(u) = \frac{\sum_{i=0}^n P_i \cdot w_i \cdot N_{i,p}(u)}{\sum_{i=0}^n w_i \cdot N_{i,p}(u)}$$

$$N_{i,0}(u) = 1 \quad \text{para} \quad u_i \leq u < u_{i+1} \\ = 0$$

$$N_{i,p}(u) = \frac{u - u_i}{u_{i+p} - u_i} N_{i,p-1}(u) + \frac{u_{i+p+1} - u}{u_{i+p+1} - u_{i+1}} N_{i+1,p-1}(u)$$

$$U = \{0, 0, \dots, 0, u_{k+1}, u_{k+2}, \dots, u_n, u_{n+1}, \dots, u_{n+k}\}$$





## Representation of Conic Shapes (1)

- A NURBS curve of the 2nd degree, with 3 points represents a conic shape if the conic form factor,  $k_c$ , defined by:

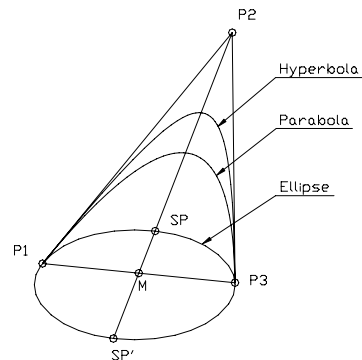
$$k_c = \frac{w_1 \cdot w_3}{4 \cdot w_2^2}$$

Has one of the following values

$$4k_c < 1.0 \Rightarrow \text{ellipse}$$

$$4k_c = 1.0 \Rightarrow \text{parabola}$$

$$4k_c > 1.0 \Rightarrow \text{hiperbole}$$



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## Representation of Conic Shapes (2)

- To represent a circular arc, the 3 control points [P1, P2, P3] must be over the vertices of a triangle isosceles
- The arc radius obtained is computed by:

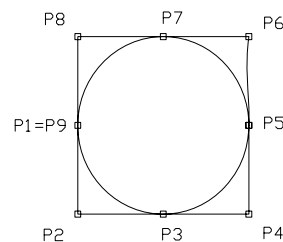
$$R = \frac{\sqrt{(1+4b^2)}}{4b} \quad \text{where:} \quad b = \frac{\sqrt{k^2-1}}{2}$$

- Complete circumferences can be represented joining arcs
- With 9 points, 4 arcs of  $90^\circ$  can be joined

$$X = \{0,0,0,0,25,0,25,0,5,0,5,0,75,0,75,1,0,1,0,1,0\}$$

$$W = \{1,0, \frac{\sqrt{2}}{2}, 1,0, \frac{\sqrt{2}}{2}, 1,0, \frac{\sqrt{2}}{2}, 1,0, \frac{\sqrt{2}}{2}, 1,0\}$$

$$P = \{P_1, P_2, P_3, P_4, P_5, P_6, P_7, P_8, P_9\}$$



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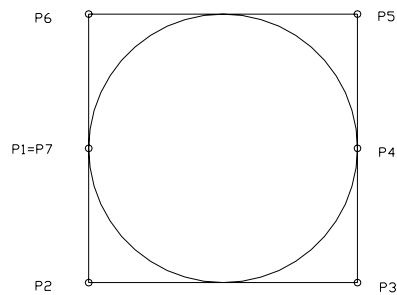
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16



## Representation of Conic Shapes (3)

- The previous representation can be simplified, removing the repeated knots 0.25 and 0.75
- The result is a circumference represented by only 7 control points



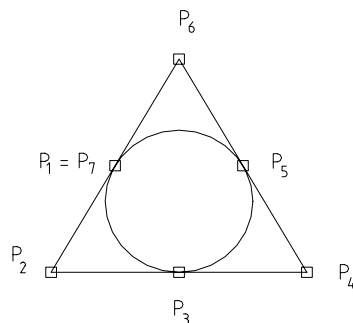
$$X = \{0,0,0,0.25,0.5,0.5,0.75,1.0,1.0,1.0\}$$

$$W = \{1.0,0.5,0.5,1.0,0.5,0.5,1.0\}$$

$$P = \{P_1, P_2, P_3, P_4, P_5, P_6, P_7\}$$

## Representation of Conic Shapes (4)

A circumference can also be obtained joining 3 arcs of  $120^\circ$ , defined by 7 control points.



$$X = \left\{0,0,0,\frac{1}{3},\frac{1}{3},\frac{2}{3},\frac{2}{3},1.0,1.0,1.0\right\}$$

$$W = \{1.0,0.5,1.0,0.5,1.0,0.5,1.0\}$$

$$P = \{P_1, P_2, P_3, P_4, P_5, P_6\}$$

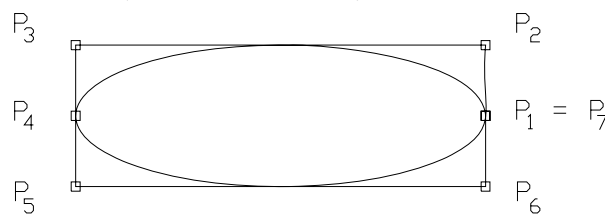
## Representation of Conic Shapes (5)

- A complete ellipse can be represented applying an affine transformation to a circumference, for example, one represented by 7 control points, keeping the distribution of the weights and the knot vector.

$$X = \{0.0, 0.0, 0.0, 0.25, 0.5, 0.5, 0.75, 1.0, 1.0, 1.0\}$$

$$W = \{1.0, 0.5, 0.5, 1.0, 0.5, 0.5, 1.0\}$$

$$P = \{P_1, P_2, P_3, P_4, P_5, P_6, P_7\}$$



## Summary - Parametric Curves (1)

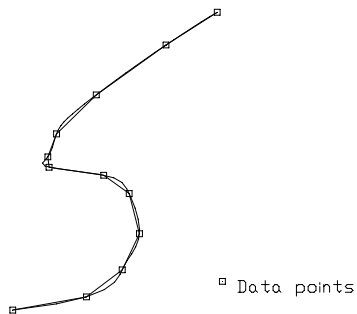
	Advantages	Disadvantages	Obs.
<b>Cubic Spline</b>	Interpolates data points	Can present unexpected inflections	
<b>Bézier</b>	The control polygon lies outside the data points	Global behavior Degree increases directly with the increasing number of control points	

## Summary - Parametric Curves (2)

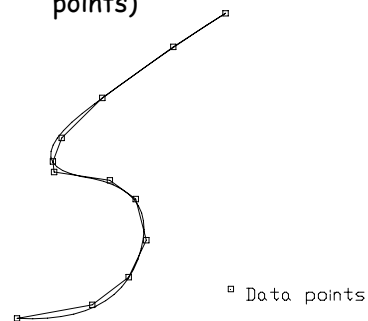
	Advantages	Disvantages	Obs.
<b>B-Spline</b>	Local behavior Degree independent of the number of control points	Can NOT represent conic shapes accurately	
<b>Beta-Spline</b>	Two additional parameters to control (bias and tension)		Used in fairing methods
<b>NURBS</b>	Accurate representation of conics	It is difficult to take advantage of the additional coordinate (weight)	State of the art. Used in most existing CAD systems

## Curve Generation

**Interpolation** (curve contains all the data points)



**Approximation** (curve tries to minimize the distance to all the data points)





## Analysis of Curve Curvature (1)

- The curvature of a space curve is defined by:

$$\kappa(t) = \frac{|x'(t) \times x''(t)|}{|x'(t)|^3}$$

- The distribution of this curvature along the curve can be represented using the method of the "porcupine"
  - vectors with modules proportional to the values of the curvature at each point
  - normal to the curve at that point
  - oriented to the opposite side of the centre of curvature

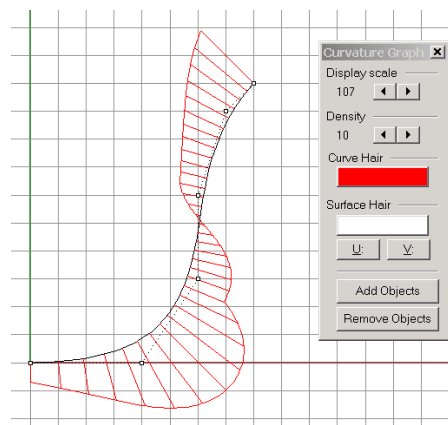
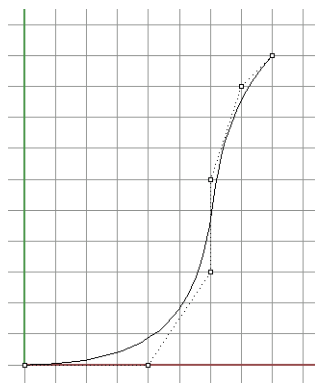
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## Analysis of Curve Curvature (2)



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## Parametric Surfaces

1. NURBS Surfaces
2. Surfaces Generation
  - Extrusion
  - Lofting
  - Sweeping
  - Revolution
  - Grid Interpolation
  - Primitives
3. Surface Analysis
  - Shading
  - Contours
  - Curvatures
  - Isophotes
  - Reflection Lines

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## NURBS Surfaces

- A NURBS surface of degree (k,l) in the directions (u,v) is defined by the expression:

$$S(u, v) = \frac{\sum_{i=0}^n \sum_{j=0}^m P_{i,j} \cdot w_{i,j} \cdot N_{i,k}(u) M_{j,l}(v)}{\sum_{i=0}^n \sum_{j=0}^m w_{i,j} \cdot N_{i,k}(u) M_{j,l}(v)}$$

$$N_{i,0}(u) = 1 \quad p/ \quad u_i \leq u < u_{i+1} \\ = 0$$

$$M_{j,0}(v) = 1 \quad p/ \quad v_j \leq v < v_{j+1} \\ = 0$$

$$N_{i,k}(u) = \frac{u - u_i}{u_{i+k} - u_i} N_{i,k-1}(u) + \\ \frac{u_{i+k} - u}{u_{i+k} - u_{i+1}} N_{i+1,k-1}(u)$$

$$M_{j,l}(v) = \frac{v - v_j}{v_{j+l} - v_j} M_{j,l-1}(v) + \\ \frac{v_{j+l} - v}{v_{j+l} - v_{j+1}} M_{j+1,l-1}(v)$$

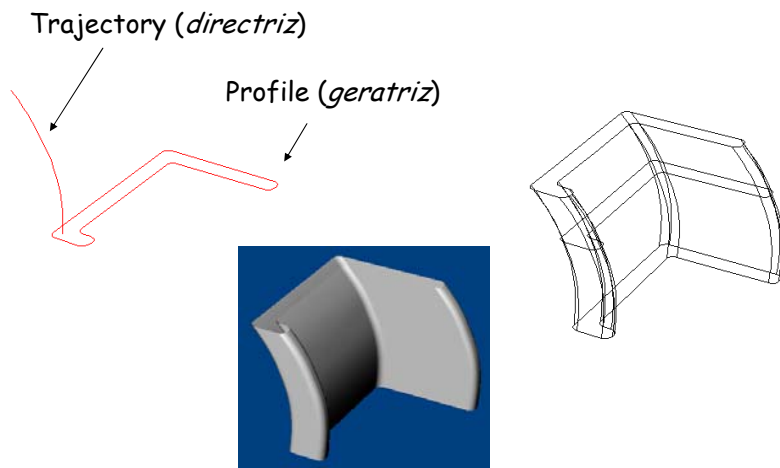
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26



## Extrusion



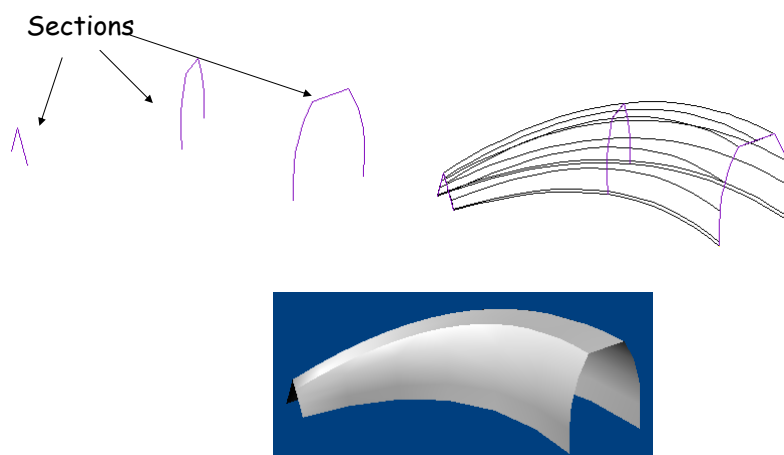
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27



## Lofting



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28

## Lofting in Shipbuilding

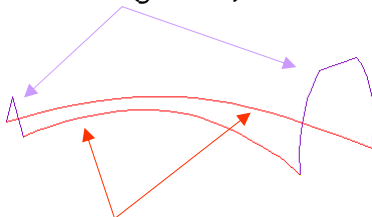
- The designation *lofting* has origin in shipbuilding
- Designates the development of the ship hull surface interpolating the shape of a set of cross sections, that was carried out in the loft room (*sala do risco*)



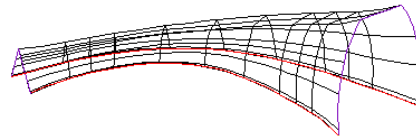
The primitive building process was similar to the modeling process, using the frames to shape the hull surface form.

## Sweeping

Profile (*geratriz*)

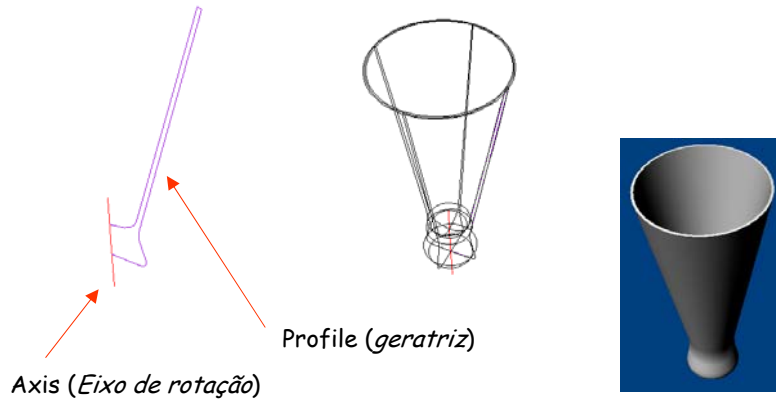


Trajectory (*directriz*)





## Surfaces of Revolution



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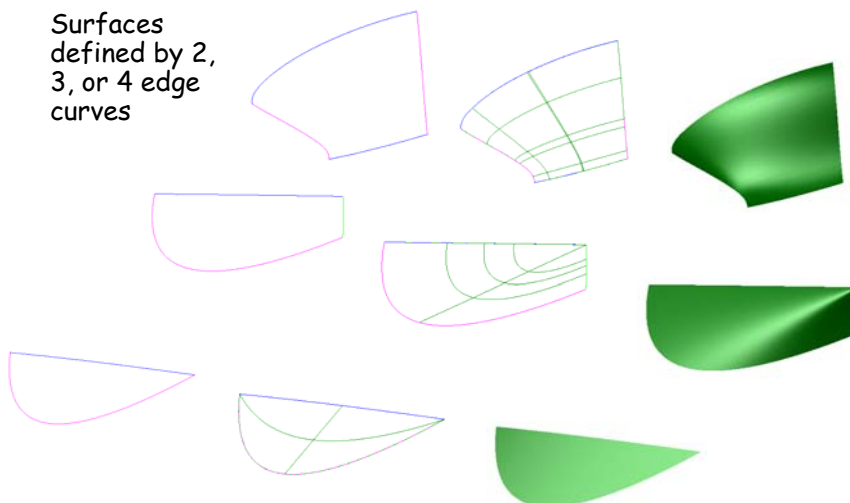
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## Edge Curves

Surfaces defined by 2, 3, or 4 edge curves



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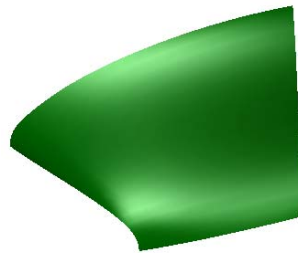
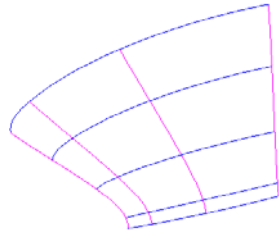
32





## Grid Interpolation

- Surface generated from a regular grid of curves
- Provide a better control over the inner shape of the surface



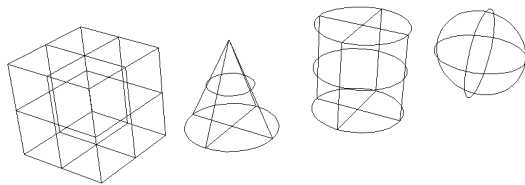
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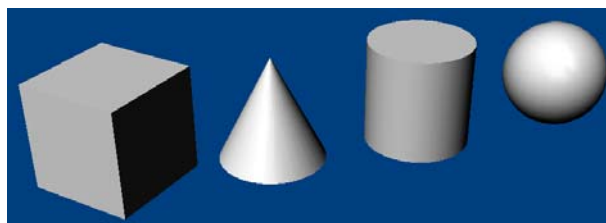
33



## Elementary Primitive Shapes



- Box
- Cone
- Cylinder
- Sphere



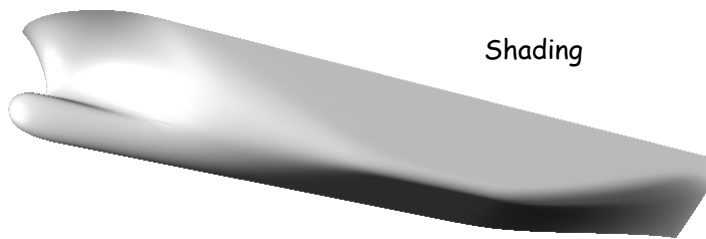
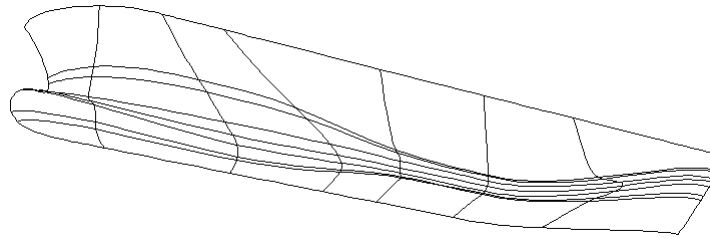
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34



## Surface Analysis - Shading



Shading

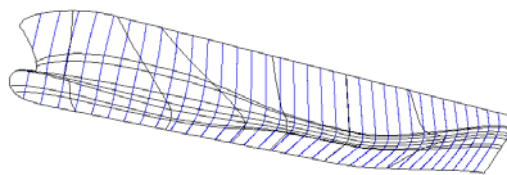
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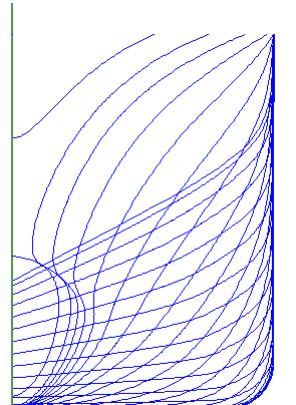
35



## Surface Analysis - Contours



Contours



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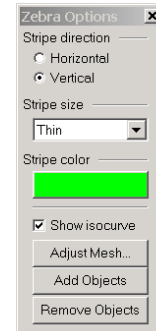
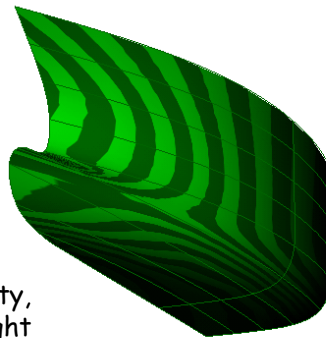
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36



## Surface Analysis - Isophotes

Isophotes:  
Analyze/Surface/Zebra



Lines of constant light intensity, created by a set of parallel light sources, with a given direction,  $L$

$$n \cdot L = \cos \alpha$$

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## Surface Analysis - Curvature

### Mean Curvature

$$H = \frac{2FM - (EN + GL)}{2(EG - F^2)}$$

### Gauss Curvature

$$K = \frac{LN - M^2}{EG - F^2}$$

### 1st Fundamental Form Coefficients

$$E = r_u \cdot r_u \quad F = r_u \cdot r_v \quad G = r_v \cdot r_v$$

### 2nd Fundamental Form Coefficients

$$L = n \cdot r_{uu} \quad M = n \cdot r_{uv} \quad N = n \cdot r_{vv}$$

Curvatures expressed as a function of the max. and min. curvatures

$$H = \frac{1}{2}(\kappa_{\min} + \kappa_{\max})$$

$$K = \kappa_{\min} \kappa_{\max}$$

Surface normal unit vector

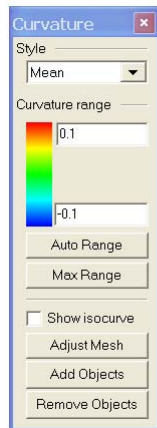
$$n = \frac{r_u \times r_v}{|r_u \times r_v|} \quad p/|r_u \times r_v| \neq 0$$

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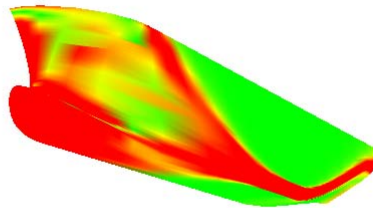
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38

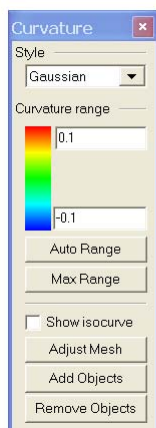
## Mean Curvature



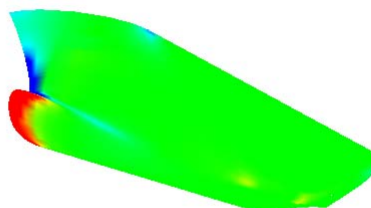
Mean Curvature distribution



## Gauss Curvature



Gauss Curvature distribution



- $K < 0$  Surface with double curvature (saddle shape)
- $K = 0$  Developable surface
- $K > 0$  Surface with single curvature (concave or convex)