

FasdHTS
TD 02.32.02.02

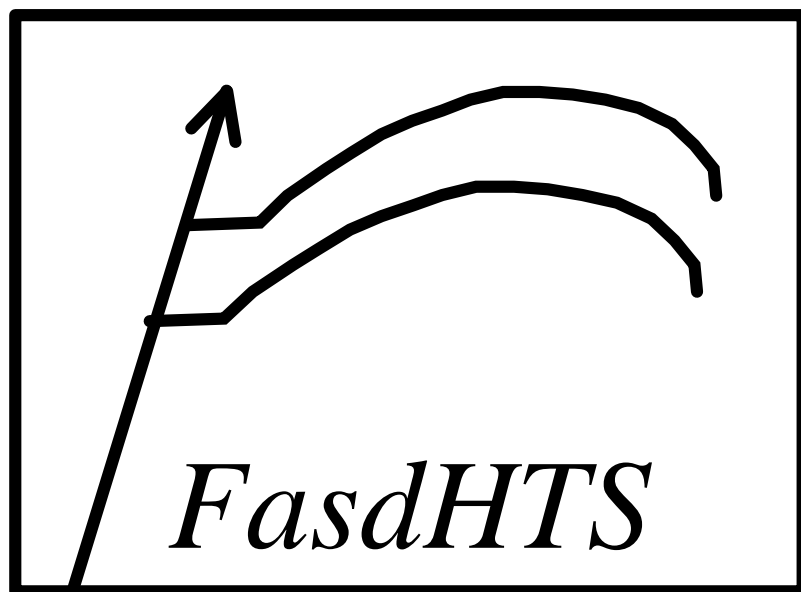
Contract: G3RD – CT 2000 - 00100

**Fabrication of the V butt welds Specimens
(Task 3.2)**



June 2002

Author : Jose Alexandre



AF – I	BV	CAT	CTH	DH	FSG	GL
GN	TUHH	IST	LIS	RS	TNO	

G3RD – CT 2000 – 00100 <i>FasdHTS</i> TD 02.32.02.02		FATIGUE BASED DESIGN RULES FOR THE APPLICATION OF HIGH TENSILE STEEL IN SHIPS			
Doc. Ref.:		Date : 21 June 2002			
TITLE :		Fabrication of Specimens (Task 3.2)			
Author :		José Alexandre			
Issued by :		LISNAVE Estaleiros Navais, S.A.			
<p>Summary:</p> <p>This report describes the design and fabrication of the Specimens for V-butt Welds, using Extra High Strength Steels, S690Q in conformity with EN 10137-2. The yield strength of this material is at least 690 N/mm². Dillinger Hütte GTS supplied all the material for these specimens.</p>					
Revision	Date	Description	Pages	Checked	Approved
0	21-06-02	Draft		EM	CR
1	23-11-02	Final		EM	CR
2	14-02-03	Final	18	EM	CR

CONTENTS

1.	Object	4
2.	Steel	4
4.	Preparation of specimens	5
5.	Welding.....	6
6.	Filler Metals: Chemical composition and mechanical properties.....	7
7.	Welding sequence	7
8.	Welding Parameters	8
9.	Welding procedure specification	8
10.	Non-destructive testing welds.....	9
11.	Experiences	9
11.1.	Preparation of the specimens	9
11.2.	Welding	9
11.3.	Economic aspects	9
12.	Conclusion	10
13.	References	10
14.	APPENDIX I.....	11
15.	APPENDIX II.....	14
16.	APPENDIX III.....	17

1. Object

The fabrication of V-butt welds specimens for thinner plates are intended for testing with 4 mm plate specimens with $L \times W = 600 \times 1200$.

2. Steel

The steel was supplied by Dillinger Hutten Werke, according with certificates in Appendix I.



3. Photo 1 – Steel plates when arrival

A summary of the mechanical properties of the steel is given in Table 1 and of the chemical composition in Table 2.

Identification mark	Steel			Heat No.	Plate No.
	Quality	Thickness	Grade		
1	DILL 690	4 mm	690 T	78874	91288
2	DILL 690	4 mm	690 T	78874	91289
3	DILL 690	4 mm	690 T	78874	91290
4	DILL 690	4 mm	690 T	78874	91291

Identification mark	Yield Stress N/mm^2	Tensile Strength N/mm^2	Elongation (%)
1, 2, 3 and 4	732	808	15

Table 1 – Mechanical properties

Identification mark	Steel		Chemical composition (%)									
	Qual.	Thick	C	Mn	Si	P	S	Cr	Ni	Mo	Al	B
1,2,3 and 4	690	4mm	0,184	1.36	0.268	0.010	0.008	0.034	0.025	0.006	0.016	0.001

Table 2 – Chemical comp osition

4. Preparation of specimens

The design proposed, as stated on document TD 01.51.01.01. Thinner plate thickness 4 mm.

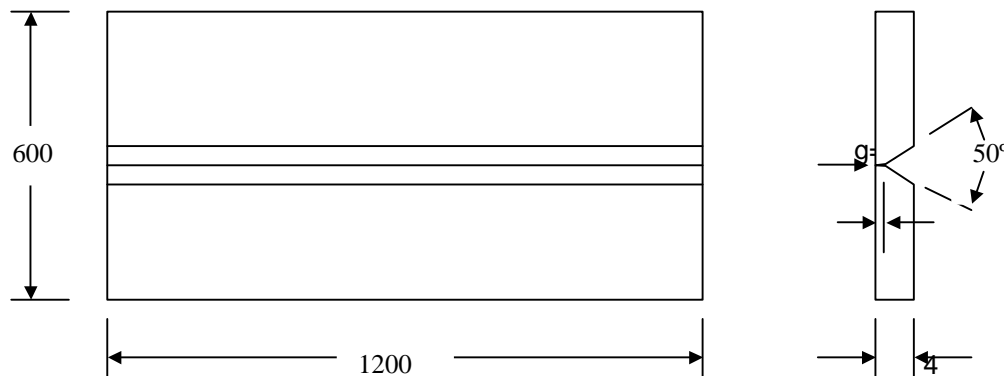


Fig.1 Welding preparation



Photo 2 – Welding preparation

The plates for the specimens were cut using steel cutting machine and grooves prepared by grinding, with an automatic machine.

To avoid plate distortion during the welding, the plates were supported by temporary reinforcements according with the sketch below (fig.2)

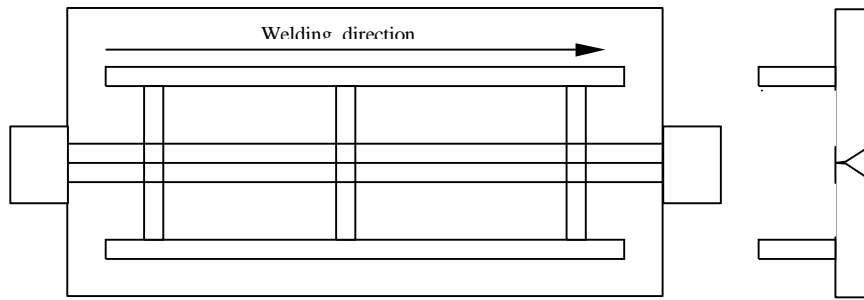


Fig. 2 Reinforcements to avoid distortion plate

After welding, the temporary reinforcements were removed, the surfaces were smooth by grinding and MPI was done to check for small cracks detection. No unacceptable indications were found.

5. Welding

An automatic machine carried out welding, as we can observe in the photos 3 and 4, using MAG process with constant current and flux-cored wire to weld the specimens. A rutile wire with a diameter of 1.2 mm was used for all the specimens.



Photo 3 – Automatic machine



Photo 4 – Welding

The same welding process and wire was used for tack welding. The welding was done in the flat position (PA) for all specimens.

To prevent start and stop defects, run-on and run-off plates was used for all specimens as shown in photos 5 and 6



Photos 5 and 6 – The use of run-on and run-off plates.

6. Filler Metals: Chemical composition and mechanical properties.

The chemical composition is shown in table 3.

Designation	Chemical composition								
	C	Mn	Si	S	P	Cr	Ni	Mo	N
H.Fluxofill42	0.068	1.413	0.297	0.007	0.013	0.495	2.247	0.486	0.003

Table 3 – Chemical composition

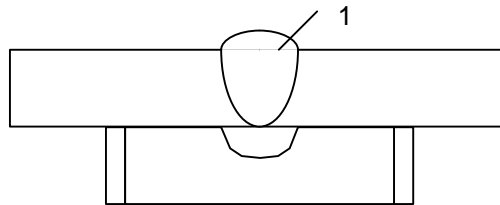
The mechanical properties are shown in table 4.

Yield Strength N/mm ²	Tensile Strength N/mm ²	Elongation (%)	Impact Strength (J)
699	782	18	12

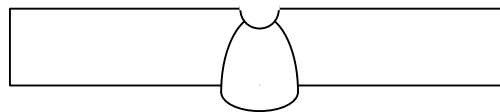
Table 4 – Mechanical properties

7. Welding sequence

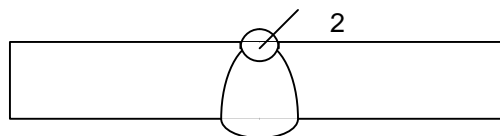
1 – Step : Face welding.



2 – Step : Grinding back side.



3 – Step: Back welding.





Photos 6 and 7 – Welding process and welding aspect

8. Welding Parameters

In table 5 is shown the welding parameters used for the specimens Model–A, without backing.

Weld Layers	Process	Filler Metal		Current		Volt Range	Travel Speed (cm/min)	Heat Input (Kj/mm)
		Class	Dia. (mm)	Type Polarity	Amp. Range			
1	Fcaw	AWS A5.29	1.2	+	229	23.6	40.3	0.80
2	Fcaw	AWS A5.29	1.2	+	229	23.6	43.1	0.75

Table 5 – Without backing

In table 6 is shown the welding parameters used for the specimens Model –B, with ceramic backing.

Weld Layers	Process	Filler Metal		Current		Volt Range	Travel Speed (cm/min)	Heat Input (Kj/mm)
		Class	Dia. (mm)	Type Polarity	Amp. Range			
1	Fcaw	AWS A5.29	1.2	+	229	23.6	31.57	1.03

Table 6 – With backing

9. Welding procedure specification

As the Yard has no experience in HTS 690 fabrication, the welding procedure specification (WPS) were developed and prepared with information obtained from DILLINGER HUTTE GTS, Technical Information No. I / 1998, in which are given some fabrication guide lines, such as:

Base metal characteristics:

Filler metals and consumables for welding DILLIMAX Steels.

Pre-heating temperature of 25°C min. for thick. below 5 mm.

Inter-pass temperature 220°C max.

No pre-heating was used to weld the 4 mm thickness plates.

The specimens were welded according with the welding procedure specification No. V.002, in Appendix I.

10. Non-destructive testing welds.

The first two, one intermediate and the last two specimens were 100% examined by X-rays, and no unacceptable indications were found.

11. Experiences

11.1. Preparation of the specimens

Differences were not found comparing to normal shipbuilding steel specimens preparation.

11.2. Welding

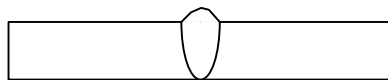
The weld ability of the flux-cored wire used is good. All specimens were welded with the same welding current and voltage. The weld beads showed a regular and good aspect.

11.3. Economic aspects

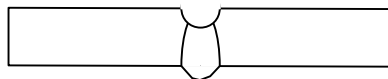
All specimens fabricated by Lisnave and sent to TUHH for testing was the type Model-A, V-butt welds.

The Model-B specimen was fabricated for comparison of times consumed purpose. The results obtained, using the parameters indicated in the Table 5.3 were as follows:

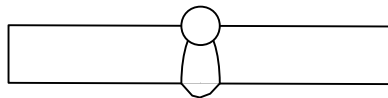
Model-A



Arc time: 3.37 minutes

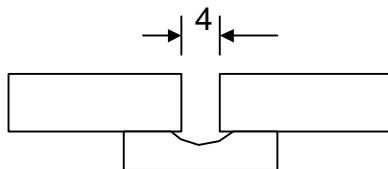


Grinding time: 2.5 minutes



Backing weld
Arc time: 3.18 minutes

Model-B



With ceramic backing
Arc time: 3.80 minutes

V-bevel preparation prepared by grinding is very time consuming.

12. Conclusion

The welding of the specimens has been done without any production problems. From the point of view of expenses, the square butt welds are preferable; a considerable time is involved in the preparation of V-bevel.

In a large scale production MAG welding process automatics with square butt welds and ceramic backing is to be considered.

13. References

1. **TNO** Programme for fatigue tests . Technical Document TD 00.51.01.01 FasdHTS
2. **DILLIMAX** – Technical Information N0.I/1998.
3. **ASME IX** – 1995 Boiler & Pressure Vessel Code

14. APPENDIX I

14.1. Welding Procedure Specification

	WELDING PROCEDURE SPECIFICATION (QW-482) ACCORDING - ASME, Section IX (See QW- 200.1)	WPS No.: SHEET No. DATE :	V-002 1 of 2 15-05-01
	SUPPORTING PQR No.		
	REVISION No.: 0 DATE: 15-05-2001		

COMPANY NAME: LISNAVE	BY:
WELDING PROCEDURE(ES): FCAW	TYPE(S): MECHANIZED <small>AUTOMATIC, MANUAL, MACHINE, OR SEMI-AUTO</small>

DETAILS

JOINTS (QW-402)

JOINT DESIGN: V-BUTT WELD GROOVE 50°

BACKING (YES): ----- (NO): NO

BACKING MATERIAL (Type)

Metal
Nonfusing Metal

Nonmetallic
Other

BASE METALS (QW-403)

P-No. 1 to P-No. 1

OR SPEC. TYPE AND GRADE: HIGH TENSILE STEEL - HTS690

TO SPEC. TYPE AND GRADE: HIGH TENSILE STEEL - HTS690

OR CH. ANALYSIS AND MECH. PROP.
TO CH. ANALYSIS AND MECH. PROP.

THICKNESS RANGE:

BASE METAL:	PLATE	GROOVE:	1.6 - 8 mm	FILLET:	ALL THICKNESS OF BASE METAL
PIPE DIA. RANGE:	NA	GROOVE:	NA	FILLET:	NA

OTHER: NA

<p>FILLER METALS (QW-404)</p> <p>SPEC. No. (SFA): A5.29 - 80</p> <p>AWS No.(CLASS): E 111TG-K3*</p> <p>F-No.: 6</p> <p>A-No.: 10</p> <p>SIZE OF FILLER METALS: Ø 1.2 mm</p> <p>WELD METAL</p> <p>THICKNESS RANGE:</p> <div style="display: flex; justify-content: space-between;"> GROOVE: 8 mm FILLET: UNLIMITED </div> <p>ELECTRODE-FLUX (CLASS): NA</p> <p>FLUX TRADE NAME: NA</p> <p>CONSUMABLE INSERT: NA</p> <p>OTHER: * Fluxofil M42 / M21 (u) "Oerlikon"</p>	<p>POSITIONS (QW-405)</p> <p>POSITION(S) OF GROOVE: 1 G</p> <p>WELDING PROGRESSION: N/A</p> <p>POSITION(S) OF FILLET: N/A</p> <hr/> <p>PREHEAT (QW-406)</p> <p>PREHEAT TEMP.: N/A</p> <p>INTERPASS TEMP. MAX.: N/A</p> <p>PREHEAT MAINTENANCE: N/A</p> <hr/> <p>POSTWELD HEAT TREATMENT (QW-407)</p> <p>TEMPERATURE RANGE: N/A</p> <p>TIME RANGE: N/A</p>
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QW-482 (Back)

WPS No:	V-002
SHEET No:	2 of 2
DATE:	15-05-01
REV.:	0

GAS (QW-408)

PERCENT COMPOSITION

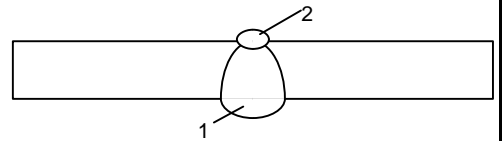
	GAS(ES)	MIXTURE	FLOW RATE
SHIELDING:	N/A	Ar+20%CO ₂	15 l/min
TRAILING.:	N/A	N/A	N/A
BACKING...:	N/A	N/A	N/A

ELECTRICAL CHARACTERISTICS (QW-409)

CURRENT AC OR DC:	DC	POLARITY:	+
AMPS (RANGE):	230	VOLTS(RANGE):	30
TUNGSTEN ELECTR. SIZE AND TYPE:	N/A <small>(PURE TUNGSTEN, 2% THORIUM, ETC.)</small>		
MODE OF METAL TRANSFER FOR GMAW:	SPRAY <small>(SPRAY ARC, SHORT CIRCUITING ARC, ETC.,)</small>		
OTHERS:	NA		

TECHNIQUE (QW-410)

STRING OR WEAWE BEAD:	STRINGER BEAD
ORIFICE OR GAS CUP SIZE:	N/A
<small>Initial and Interpass Cleaning (Brushing, Grinding, etc.)</small>	GRINDING
METHOD OF BACK GOUGING:	GRINDING
OSCILLATION:	N/A
CONTACT TUBE TO WORK DISTANCE:	N/A
MULTIPLE OR SINGLE PASS (PER SIDE):	SINGLE PASS
MULTIPLE OR SINGLE ELECTRODES:	SINGLE
TRAVEL SPEED (RANGE):	40cm/min
PEENING:	N/A
OTHER:	N/A

DETAILS IDENTIFICATION OF PASSES

WELD LAYERS	PROCESS	FILLER METAL		CURRENT		VOLT RANGE	TRAVEL SPEED RANGE	OTHER (EG., REMARKS, COMMENTS, HOT WIRE, ADDITION, TECHNIQUE, TORCH ANGLE, ETC.,)
		CLASS	DIAM.	TYPE POLAR.	AMPS RANGE			
1 & 2	FCAW	E 111TG-K3	1.2	DC +	230	30	40	ALL VALUES +/- 10%

ORGANISATION: **LISNAVE**

APPROVED BY:

DATE: 2001/02/22

 Jose Alexandre
 SIGN / STAMP

DATE:

SIGN / STAMP

15.APPENDIX II

15.1.Steel Plate Certificates



Richard A. Long, Jr.
 Chairman, Board of Directors
 1994-1995

CONCENTRATION PROCESS	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
CONCENTRATION PROCESS	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100

INSPECTION CERTIFICATE

Case	Age	Sex	Occupation	Duration of symptoms	Location of symptoms	Severity of symptoms	Response to treatment	Outcome
1	45	Male	Teacher	10 years	Right arm	Mild	Good	Recovery
2	52	Female	Homemaker	5 years	Left hand	Moderate	Fair	Recovery
3	60	Male	Engineer	15 years	Right hand	Severe	Poor	No recovery
4	38	Female	Nurse	8 years	Left arm	Mild	Good	Recovery
5	55	Male	Farmer	12 years	Right hand	Moderate	Fair	Recovery
6	42	Female	Teacher	7 years	Left hand	Mild	Good	Recovery
7	65	Male	Retired	20 years	Right arm	Severe	Poor	No recovery
8	35	Female	Homemaker	3 years	Left hand	Mild	Good	Recovery
9	58	Male	Engineer	18 years	Right hand	Severe	Poor	No recovery
10	48	Female	Nurse	11 years	Left arm	Moderate	Fair	Recovery

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2000-2001

Project	Year	Value	Source
1. Construction of a new school building	2010	100,000	Local Government
2. Purchase of a new bus	2011	50,000	Private Donor
3. Renovation of the library	2012	75,000	Government Grant
4. Purchase of a new computer system	2013	30,000	Local Business
5. Construction of a new playground	2014	120,000	Community Fund
6. Purchase of a new car	2015	40,000	Local Government
7. Renovation of the sports field	2016	90,000	Private Donor
8. Purchase of a new printer	2017	20,000	Local Business
9. Construction of a new office building	2018	200,000	Government Grant
10. Purchase of a new van	2019	60,000	Local Government

[illegible][illegible]

Case	Age	Sex	Occupation	Duration	Location	Outcome
1	25	M	Student	10 days	Home	Recovered
2	30	F	Teacher	15 days	Home	Recovered
3	35	M	Engineer	20 days	Home	Recovered
4	40	F	Homemaker	25 days	Home	Recovered
5	45	M	Manager	30 days	Home	Recovered
6	50	F	Retired	35 days	Home	Recovered
7	55	M	Farmer	40 days	Home	Recovered
8	60	F	Teacher	45 days	Home	Recovered
9	65	M	Engineer	50 days	Home	Recovered
10	70	F	Homemaker	55 days	Home	Recovered
11	75	M	Manager	60 days	Home	Recovered
12	80	F	Retired	65 days	Home	Recovered
13	85	M	Farmer	70 days	Home	Recovered
14	90	F	Teacher	75 days	Home	Recovered
15	95	M	Engineer	80 days	Home	Recovered
16	100	F	Homemaker	85 days	Home	Recovered
17	105	M	Manager	90 days	Home	Recovered
18	110	F	Retired	95 days	Home	Recovered
19	115	M	Farmer	100 days	Home	Recovered
20	120	F	Teacher	105 days	Home	Recovered

IN CASE OF AN INTERNAL STRESS-RELIEVING HEAT TREATMENT THE PLATE MAINTAINS THE STRESS-RELIEVED STATE. ON THE OTHER HAND, AS THE MS IS COOLING, THE STRESS-RELIEVED STATE IS NOT MAINTAINED.

[illegible]

Dr. HILL, JR.



Information under this heading is for reference only and does not constitute a recommendation.

600 ANALYSIS REPORT NO. 13
 ANALYSIS OF RECEIVED 5.1.8 85 18204 - 85 18204 - 218 18204
 ANALYSIS OF RECEIVED 5.1.8 85 18204 - 85 18204 - 218 18204
 ANALYSIS OF RECEIVED 5.1.8 85 18204 - 85 18204 - 218 18204

600 ANALYSIS REPORT NO. 13
 ANALYSIS OF RECEIVED 5.1.8 85 18204 - 85 18204 - 218 18204
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600 - 800 PROPERTY IDENTIFICATION

Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name
01	5.1.8 85 18204	02	5.1.8 85 18204	03	5.1.8 85 18204	04	5.1.8 85 18204	05	5.1.8 85 18204
06	5.1.8 85 18204	07	5.1.8 85 18204	08	5.1.8 85 18204	09	5.1.8 85 18204	10	5.1.8 85 18204
11	5.1.8 85 18204	12	5.1.8 85 18204	13	5.1.8 85 18204	14	5.1.8 85 18204	15	5.1.8 85 18204
16	5.1.8 85 18204	17	5.1.8 85 18204	18	5.1.8 85 18204	19	5.1.8 85 18204	20	5.1.8 85 18204

800 - 900 MARKING

ITEM NO. 13
 STEEL GRADE DILLINGER-800
 MARK NO. 13

900 - 920 TENSILE TEST

Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name
01	5.1.8 85 18204	02	5.1.8 85 18204	03	5.1.8 85 18204	04	5.1.8 85 18204	05	5.1.8 85 18204
06	5.1.8 85 18204	07	5.1.8 85 18204	08	5.1.8 85 18204	09	5.1.8 85 18204	10	5.1.8 85 18204
11	5.1.8 85 18204	12	5.1.8 85 18204	13	5.1.8 85 18204	14	5.1.8 85 18204	15	5.1.8 85 18204
16	5.1.8 85 18204	17	5.1.8 85 18204	18	5.1.8 85 18204	19	5.1.8 85 18204	20	5.1.8 85 18204

920 - 940 CHEMICAL COMPOSITION

Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name
01	5.1.8 85 18204	02	5.1.8 85 18204	03	5.1.8 85 18204	04	5.1.8 85 18204	05	5.1.8 85 18204
06	5.1.8 85 18204	07	5.1.8 85 18204	08	5.1.8 85 18204	09	5.1.8 85 18204	10	5.1.8 85 18204
11	5.1.8 85 18204	12	5.1.8 85 18204	13	5.1.8 85 18204	14	5.1.8 85 18204	15	5.1.8 85 18204
16	5.1.8 85 18204	17	5.1.8 85 18204	18	5.1.8 85 18204	19	5.1.8 85 18204	20	5.1.8 85 18204

940 - 960 CARBON EQUIVALENT FORMULA / ALLOWING DETECTIONS

Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name	Item No.	Item Name
01	5.1.8 85 18204	02	5.1.8 85 18204	03	5.1.8 85 18204	04	5.1.8 85 18204	05	5.1.8 85 18204
06	5.1.8 85 18204	07	5.1.8 85 18204	08	5.1.8 85 18204	09	5.1.8 85 18204	10	5.1.8 85 18204
11	5.1.8 85 18204	12	5.1.8 85 18204	13	5.1.8 85 18204	14	5.1.8 85 18204	15	5.1.8 85 18204
16	5.1.8 85 18204	17	5.1.8 85 18204	18	5.1.8 85 18204	19	5.1.8 85 18204	20	5.1.8 85 18204



667

16.APPENDIX III

16.1.Welding Consumable Data

